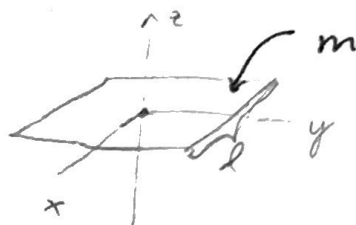


Rigid body in 3-D

8.1

Write $\underline{I}$ for plate



10 $I_{xx} = \int (y^2 + z^2) dm$ but $z=0$

$\rho = \frac{m}{l^2}$

$$= 2 \int_0^{l/2} y^2 (l dy \rho) = \frac{2}{3} y^3 \frac{l m}{l^2} \Big|_0^{l/2} = \underline{\underline{\frac{l^2 m}{12}}}$$

$I_{yy} = I_{xx} = \underline{\underline{\frac{l^2 m}{12}}}$

$\underline{\underline{I_{zz}}} = I_{xx} + I_{yy} = \frac{2l^2 m}{12} = \underline{\underline{\frac{l^2 m}{6}}}$

$I_{yx} = I_{xy} = - \int xy dm = - \int_{-l/2}^{l/2} \int_{-l/2}^{l/2} xy dx dy \rho = -\rho \int_{-l/2}^{l/2} y dy \left[\frac{x^2}{2} \right]_{-l/2}^{l/2} = 0$

So

$\underline{I} = l^2 m \begin{bmatrix} \frac{1}{12} & 0 & 0 \\ 0 & \frac{1}{12} & 0 \\ 0 & 0 & \frac{1}{6} \end{bmatrix} \checkmark$

8.2

find $\underline{I}$ & T when it rotates about a diagonal:

10 $\vec{\omega} = \frac{\omega}{\sqrt{2} l^2} \begin{bmatrix} l \\ l \\ 0 \end{bmatrix} = \frac{\omega}{\sqrt{2}} \begin{bmatrix} 1 \\ 1 \\ 0 \end{bmatrix}$

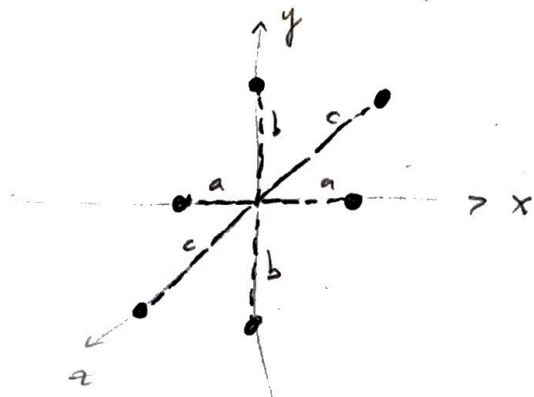
same direction $\vec{\omega}$

$\underline{L} = \underline{I} \vec{\omega} = \frac{l^2 m}{\sqrt{2} 12} \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 2 \end{bmatrix} \begin{bmatrix} 1 \\ 1 \\ 0 \end{bmatrix} \omega = \underline{\underline{\frac{m l^2 \omega}{12 \sqrt{2}} \begin{bmatrix} 1 \\ 1 \\ 0 \end{bmatrix} \checkmark}}$

$T = \frac{1}{2} \omega^T \underline{L} = \frac{1}{2} \left[\frac{\omega}{\sqrt{2}} [1, 1, 0] \right] \begin{bmatrix} 1 \\ 1 \\ 0 \end{bmatrix} \frac{m l^2 \omega}{12 \sqrt{2}} = \frac{\omega^2 l^2 m}{12 \cdot 2} \checkmark$

$\underline{\underline{T = \frac{\omega^2 l^2 m}{24} \checkmark}}$

8.3



Show if coord, coincide with rods, they are principal axes, write down the inertia tensor.

by symmetry it can be shown body axes are principal axes. But the results of $\mathbb{I}$ will reveal it.

$$\begin{aligned} \bullet I_{xx} &= \sum_i (y_i^2 + z_i^2) m_i = m [0^2 + 0^2 + (b^2) + (-b)^2 + c^2 + (-c)^2] \\ &= \underline{2m(b^2 + c^2)} \end{aligned}$$

$$\begin{aligned} \bullet I_{yy} &= \sum_i (x_i^2 + z_i^2) m_i = m [a^2 + a^2 + 0 + 0 + c^2 + c^2] \\ &= \underline{2m(a^2 + c^2)} \end{aligned}$$

$$\bullet \text{ similar for } I_{zz} \quad \text{ie } \underline{I_{zz} = 2m(b^2 + a^2)}$$

$$\bullet \underline{I_{xy} = I_{yx}} = -\sum x_i y_i m_i = -m [0 + 0 + 0 + \dots] = \underline{0}$$

$$\text{similar } I_{yz}, I_{zy}, I_{xz}, I_{zx} = 0$$

$$\text{So } \mathbb{I} = 2m \begin{bmatrix} b^2 + c^2 & 0 & 0 \\ 0 & a^2 + c^2 & 0 \\ 0 & 0 & b^2 + a^2 \end{bmatrix}$$

because this is a diagonal matrix, ie.

$$L_{xx}, L_{yy}, L_{zz} \neq 0$$

its coincident with principal axes ✓

8.4

Find the $\vec{L}$ & T of 8.3 when rot. about axis $\vec{OP}$ where $P = (a, b, c)$ at speed ω



$$\vec{\omega} = \omega \begin{bmatrix} a \\ b \\ c \end{bmatrix} \frac{1}{\sqrt{a^2 + b^2 + c^2}}$$

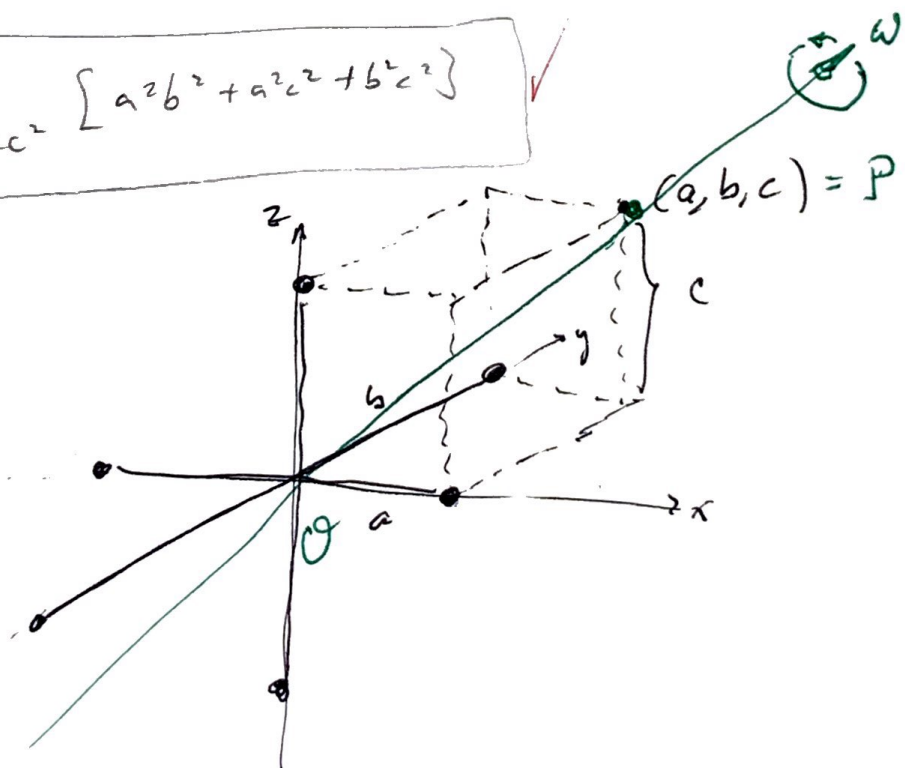
$$\vec{L} = \vec{I} \vec{\omega} = \frac{2m\omega}{\sqrt{a^2 + b^2 + c^2}} \begin{bmatrix} b^2 + c^2 & 0 & 0 \\ 0 & a^2 + c^2 & 0 \\ 0 & 0 & a^2 + b^2 \end{bmatrix} \begin{bmatrix} a \\ b \\ c \end{bmatrix}$$

$$\vec{L} = \frac{2m\omega}{\sqrt{a^2 + b^2 + c^2}} \begin{bmatrix} a(b^2 + c^2) \\ b(a^2 + c^2) \\ c(a^2 + b^2) \end{bmatrix} \quad \checkmark$$

$$T = \frac{1}{2} \vec{\omega} \cdot \vec{L} = \frac{1}{2} \frac{\omega}{\sqrt{a^2 + b^2 + c^2}} \begin{bmatrix} a(b^2 + c^2) \\ b(a^2 + c^2) \\ c(a^2 + b^2) \end{bmatrix} \cdot \frac{2\omega}{\sqrt{a^2 + b^2 + c^2}}$$

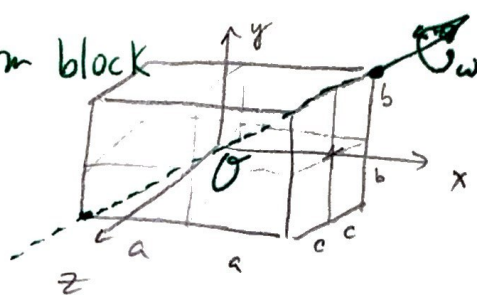
$$= \frac{m\omega^2}{a^2 + b^2 + c^2} \left[a^2(b^2 + c^2) + b^2(a^2 + c^2) + c^2(a^2 + b^2) \right]$$

$$T = \frac{2m\omega^2}{a^2 + b^2 + c^2} \left[a^2b^2 + a^2c^2 + b^2c^2 \right] \quad \checkmark$$



8.5

uniform block



(a) Find $\mathbb{I}$

CM @ (0,0,0)

$$I_{xx} = \int (y^2 + z^2) dm = \rho \int y^2 dy dx dz + \rho \int z^2 dz dy dx$$

$$= \rho \frac{y^3}{3} \Big|_{-b}^b \times \int_{-a}^a z \Big|_{-c}^c + \rho \frac{z^3}{3} \Big|_{-c}^c \int_{-b}^b y \Big|_{-a}^a$$

$$\rho = \frac{m}{2abc}$$

$$= \rho \left[\frac{2}{3} b^3 2a 2c + \frac{2}{3} c^3 2b 2a \right] = \frac{m}{3} [b^2 + c^2]$$

I_{yy} is cyclically similar to I_{xx} (exchange $y \rightarrow z, z \rightarrow x$
or $b \rightarrow c, c \rightarrow a$)

so
$$I_{yy} = \frac{m}{3} [c^2 + a^2]$$

similarly
$$I_{zz} = \frac{m}{3} [a^2 + b^2]$$

$$I_{xy} = -\rho \int xy dx dy dz = \frac{\rho}{2} \left[\frac{y^2}{2} \right]_{-a}^a \Big|_{-b}^b \Big|_{-c}^c$$

2nd order, symmetry $\Rightarrow 0$

similar for I_{yz}, I_{xz}

so

$$\mathbb{I} = \frac{m}{3} \begin{bmatrix} b^2 + c^2 & 0 & 0 \\ 0 & a^2 + c^2 & 0 \\ 0 & 0 & a^2 + b^2 \end{bmatrix} \checkmark$$

8.5 cont) if $\vec{n} = OP$ $P = (a, b, c)$

then $\omega = \frac{W}{\sqrt{a^2 + b^2 + c^2}} \begin{bmatrix} a \\ b \\ c \end{bmatrix}$

$$L = \frac{m}{3} \begin{bmatrix} b^2 + c^2 & 0 & 0 \\ 0 & a^2 + c^2 & 0 \\ 0 & 0 & b^2 + a^2 \end{bmatrix} \begin{bmatrix} a \\ b \\ c \end{bmatrix} \frac{W}{\sqrt{a^2 + b^2 + c^2}}$$

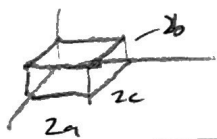
$$L = \frac{Wm}{3\sqrt{a^2 + b^2 + c^2}} \begin{bmatrix} a(b^2 + c^2) \\ b(a^2 + c^2) \\ c(b^2 + a^2) \end{bmatrix}$$

$$T = \frac{1}{2} \omega^T L = \frac{1}{2} \left(\frac{W}{\sqrt{a^2 + b^2 + c^2}} \right) \left(\frac{Wm}{3\sqrt{a^2 + b^2 + c^2}} \right) [a, b, c] \begin{bmatrix} ac & 1 \\ bc &) \\ ca &) \end{bmatrix}$$

$$= \frac{W^2 m}{2 \cdot 3(a^2 + b^2 + c^2)} \{a^2(b^2 + c^2) + b^2(a^2 + c^2) + c^2(b^2 + a^2)\}$$

$$T = \frac{W^2 m}{3(a^2 + b^2 + c^2)} [a^2 b^2 + b^2 c^2 + c^2 a^2]$$

(b) for origin @ a corner:



$$I_{xx} = \int y^2 + z^2 \rho dx dy dz$$

$$= \rho \left[\frac{y^3}{3} \right]_0^{2b} \left[\frac{z^2}{2} \right]_0^{2c} \times \left[\frac{x^2}{2} \right]_0^{2a} + \rho \left[\frac{z^3}{3} \right]_0^{2c} \times \left[\frac{y^2}{2} \right]_0^{2b} \times \left[\frac{x^2}{2} \right]_0^{2a}$$

$$= \left(\frac{m}{8abc} \right) \left[\frac{8b^3}{3} \frac{2c}{2} \frac{2a}{2} + \frac{8c^3}{3} \frac{2a}{2} \frac{2b}{2} \right] = \frac{4m}{3} [a^2 + b^2]$$

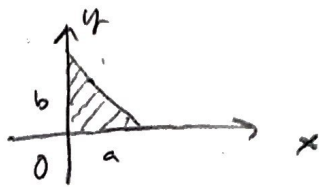
similarly $I_{yy} = \frac{4}{3} m [a^2 + c^2]$, $I_{zz} = \frac{4}{3} m [a^2 + b^2]$

$$I_{xy} = -\int xy dx dy dz = -\rho \left[\frac{x^2}{2} \right]_0^{2a} \left[\frac{y^2}{2} \right]_0^{2b} \left[\frac{z^2}{2} \right]_0^{2c} = \left(\frac{-m}{8abc} \right) \frac{4a^2 4b^2 2c}{4} = -mab$$

similarly for $I_{yz} = -mbc$, $I_{xz} = -mac$.

$$I = m \begin{bmatrix} \frac{4}{3}(b^2 + c^2) & -ab & -ac \\ -ab & \frac{4}{3}(a^2 + c^2) & -bc \\ -ac & -bc & \frac{4}{3}(a^2 + b^2) \end{bmatrix}$$

8.6 @ Find I for a triangle



$$y = -\frac{b}{a}x + b$$

• $I_{xx} = \rho \int (y^2 + z^2) dx dy$ but $z=0$ $I_{xx} = \rho \int y^2 dx dy = \rho \int_0^a \int_0^{-\frac{b}{a}x+b} y^2 dy dx$

$$= \rho \int_0^a \left(-\frac{b}{a}x + b \right)^3 dx \quad \text{let } u = -\frac{b}{a}x + b \quad du = -\frac{b}{a} dx$$

$$= \rho \left(\frac{a}{b} \right) \int_0^b \frac{u^3}{3} du = \frac{\rho a}{b} \frac{b^4}{3 \cdot 4} = \left(\frac{m}{\frac{1}{2}ab} \right) \frac{a b^3}{12} = \frac{1}{6} m b^2$$

• $I_{yy} = \rho \int (x^2 + z^2) dx dy$ but $z=0$ $I_{yy} = \rho \int_0^b \int_0^{(y-b)a/b} x^2 dx dy = \frac{\rho a^3}{6} \int_0^b \frac{(y-b)^3}{3} dy$

$$= \left(\frac{m}{\frac{1}{2}ab} \right) \frac{1}{3} \frac{a^3}{3} \frac{b^4}{4} = \frac{m a^3}{6a} = \frac{m a^2}{6}$$

• by $\perp$ axis theorem

$$\underline{I_{zz}} = I_{xx} + I_{yy} = \frac{m}{6} (a^2 + b^2)$$

• $I_{xz}, I_{yz} = 0$

$$I_{xy} = -\rho \int xy dx dy = \rho \int_0^a \int_0^{-\frac{b}{a}x+b} xy dy dx$$

$$= -\frac{m}{\left(\frac{1}{2}ab \right)} \int_0^a x dx \left[\frac{\left(-\frac{b}{a}x + b \right)^2}{2} \right] = - \int_0^a x \left[\frac{b^2}{a^2} x^2 + 2 \frac{b^2}{a} x + b^2 \right] dx$$

$$= - \left(\frac{b^2}{a^2} \frac{a^4}{4} + 2 \frac{b^2}{a} \frac{a^3}{3} + \frac{b^2}{2} a \right) \rho = -b^2 a^2 \left[\frac{1}{4} + \frac{2}{3} + \frac{1}{2} \right] \rho = -b^2 a^2 \left(\frac{1}{12} \right) \rho = \frac{2m}{ab} \left(\frac{b^2 a^3}{12} \right)$$

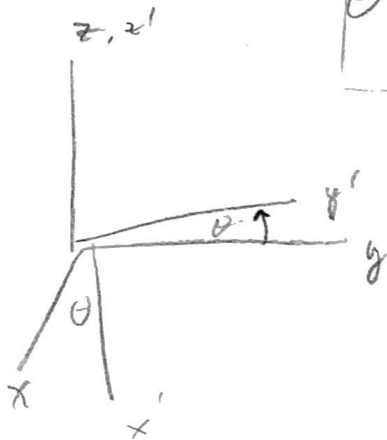
$$I_{xy} = -\frac{mab}{6}$$

$$\underline{I} = \frac{m}{6} \begin{bmatrix} b^2 & -ab/2 & 0 \\ -ab/2 & a^2 & 0 \\ 0 & 0 & a^2 + b^2 \end{bmatrix}$$

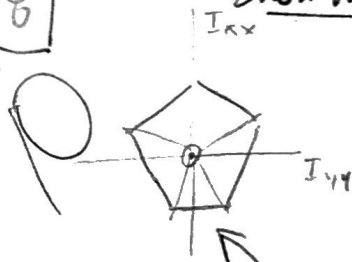
(8.6 cont) (b) Find principle axii (eigenvectors of $\mathbb{I}$) if non-lamina object

For lamina (plane) $\tan 2\theta = \frac{2 I_{xy}}{I_{xx} - I_{yy}} = \frac{-2ab}{a^2 - b^2}$

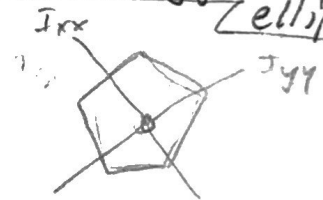
$$\theta = \frac{\tan^{-1} \left(\frac{2ab}{b^2 - a^2} \right)}{2}$$



8.8 Show momental ellipsoid of lamina regular polygon is an ellipsoid.



if we turn $\frac{2\pi}{n}$ Radians



here I_{xx} is symmetrical (a principal axis)

now if the lamina polygon is uniform mass, the C.M. is coincident with the geometric center.

Turn $\frac{2\pi}{n}$ about this C.M., now I_{yy} is the "balanced" I . Another $\frac{2\pi}{n}$ yields the same as the initial condition, back to I_{xx} .

i.e. I_{xx} & I_{yy} are cyclical exchangeable.

over
→

so in $x^2 I_{xx} + y^2 I_{yy} + z^2 I_{zz} = 1$ is cyclical in x^2, y^2, z^2

component stress in a rotating body

So initial axes yield.

Exhaustion
(unhappy)

$$x^2 I_{0xx} + y^2 I_{0yy} + z^2 I_{0zz} = 1$$

1st term

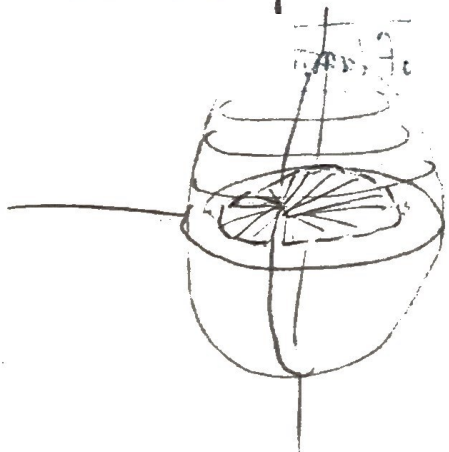
$$x^2 I_{0yy} + y^2 I_{0xx} + z^2 I_{0zz} = 1$$

2nd

$$x^2 I_{0xx} + y^2 I_{0yy} + z^2 I_{0zz} = 1$$

for a circle $ax^2 + by^2 \Rightarrow a = b^*$

so ellipsoid is circular in x, y plane.



NOY WERICKSON

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B.1-6, B

Dec 2, 1961

* let $I_{zz} = I_{xx} + I_{yy}$ by + - x, y

$$x^2(I_{xx}) + y^2 I_{yy} + z^2 I_{zz} = 1$$

$$x^2(I_{zz} - I_{yy}) + y^2 I_{yy} + z^2 I_{zz} = 1$$

$$x^2 I_{zz} - x^2 I_{yy} + y^2 I_{yy} + z^2 I_{zz} = 1$$

$$(-x^2 + y^2) I_{yy} + (z^2 + x^2) I_{zz} = 1$$

let $z=0$ to examine a plane section

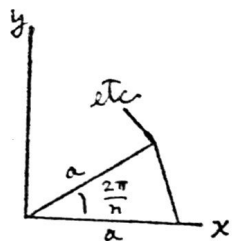
$$(-x^2 + y^2) I_{yy} + x^2 I_{zz} = 1$$

$$x^2(I_{zz} - I_{yy}) + y^2 I_{yy} = 1$$

Excellent work

please see the key for a good math proof.

- 8.8) An n -gon is composed of n triangles, each with two sides of length a and angle between them $\frac{2\pi}{n}$.



Take $z \perp$ plane of lamina, x along a side of a triangle, as shown.

There will be $\frac{n}{2}$ triangles for $y > 0$ and $\frac{n}{2}$ for $y < 0$.

$\Rightarrow \underline{I_{xy} = 0}$. So we have principal axes.

$$I_{zz} = I_{xx} + I_{yy}$$

The n -gon has an n -fold axis of symmetry along z .

So if we rotate axes by $\frac{2\pi k}{n}$, $I_{x'x'} = I_{xx}$ and $I_{y'y'} = I_{yy}$.

$\Rightarrow$ Momental ellipsoid has an n -fold axis of symmetry

along z . The only way an ellipsoid can have an n -fold axis with $n > 2$ is if it is an ellipsoid of revolution.

Proof:

For our axes the momental ellipsoid is given by

$$x^2 I_{xx} + y^2 I_{yy} + z^2 I_{zz} = 1.$$

$$\vec{r}^T \underline{\underline{I}} \vec{r} = 1$$

We can rotate axes by $\theta = \frac{2\pi k}{n}$ by the orthogonal transformation

$$\underline{\underline{S}} = \begin{pmatrix} \cos \theta & \sin \theta & 0 \\ -\sin \theta & \cos \theta & 0 \\ 0 & 0 & 1 \end{pmatrix}. \quad (\text{See p. 19 of text.})$$

$$\vec{r}' = \underline{\underline{S}} \vec{r}, \quad \underline{\underline{S}}^{-1} = \underline{\underline{S}}^T, \quad \vec{r}'^T = \vec{r}^T \underline{\underline{S}}^T \Rightarrow \vec{r} = \underline{\underline{S}}^T \vec{r}'$$

$$\vec{r}^T = \vec{r}'^T \underline{\underline{S}}$$

$$\Rightarrow \vec{r}'^T \underline{\underline{S}} \underline{\underline{I}} \underline{\underline{S}}^T \vec{r}' = 1$$

$\Rightarrow \underline{\underline{I}}' = \underline{\underline{S}} \underline{\underline{I}} \underline{\underline{S}}^T = \underline{\underline{I}}$ since we are rotating about an n -fold axis of symmetry.

(8.8 continued)

$$\underline{\underline{I}} \underline{\underline{S}}^T = \begin{pmatrix} I_{xx} & 0 & 0 \\ 0 & I_{yy} & 0 \\ 0 & 0 & I_{zz} \end{pmatrix} \begin{pmatrix} \cos \theta & -\sin \theta & 0 \\ \sin \theta & \cos \theta & 0 \\ 0 & 0 & 1 \end{pmatrix} = \begin{pmatrix} I_{xx} \cos \theta & -I_{xx} \sin \theta & 0 \\ I_{yy} \sin \theta & I_{yy} \cos \theta & 0 \\ 0 & 0 & I_{zz} \end{pmatrix}$$

$$\begin{aligned} \underline{\underline{I}}' &= \underline{\underline{S}} \underline{\underline{I}} \underline{\underline{S}}^T = \begin{pmatrix} \cos \theta & \sin \theta & 0 \\ -\sin \theta & \cos \theta & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} I_{xx} \cos \theta & -I_{xx} \sin \theta & 0 \\ I_{yy} \sin \theta & I_{yy} \cos \theta & 0 \\ 0 & 0 & I_{zz} \end{pmatrix} \\ &= \begin{pmatrix} I_{xx} \cos^2 \theta + I_{yy} \sin^2 \theta & (I_{yy} - I_{xx}) \sin \theta \cos \theta & 0 \\ (I_{yy} - I_{xx}) \sin \theta \cos \theta & I_{xx} \sin^2 \theta + I_{yy} \cos^2 \theta & 0 \\ 0 & 0 & I_{zz} \end{pmatrix} \end{aligned}$$

$$\underline{\underline{I}}' = \underline{\underline{I}} \Rightarrow (I_{yy} - I_{xx}) \sin \theta \cos \theta = 0$$

$$\Rightarrow I_{xx} = I_{yy} \quad \text{or} \quad \sin \theta \cos \theta = \frac{1}{2} \sin 2\theta = 0$$

if $2\theta \neq n\pi$, then $I_{xx} = I_{yy}$ and the ellipsoid is one of revolution.

$$\text{But } \theta = \frac{2\pi k}{n}, \quad k=1, \dots, n.$$

$$\Rightarrow 2\theta = \frac{4k}{n} \pi$$

$n \geq 3$. So if $n=3$, $k=1 \Rightarrow I_{xx} = I_{yy}$.

if $n=4$ we have a square and

$I_{xx} = I_{yy}$ by symmetry.

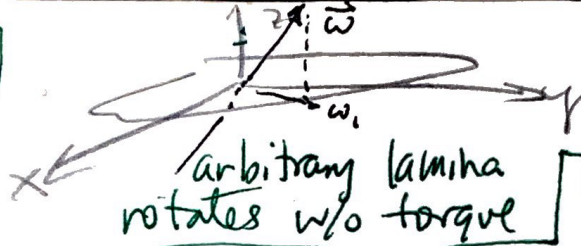
if $n > 4$ but not a multiple of 4, $2\theta \neq n\pi$ for some symmetry rotations.

if n is a multiple of 4, the four quadrants have identical mass distributions, so

$I_{xx} = I_{yy}$ by symmetry.

$\therefore I_{xx} = I_{yy}$ for all n -gons, $n \geq 3$. $\Rightarrow$ Momental ellipsoid is one of revolution.

8.10



$\omega_1^2 = \omega_x^2 + \omega_y^2$
 show $\omega_1 = \text{const.}$ but $\omega_z \neq \text{const.}$
 we need to show $\omega_1^2 = \text{const.}$

or $\omega_x^2 + \omega_y^2 = \text{const.}$

or it's derivative = 0

$2\omega_x \dot{\omega}_x + 2\omega_y \dot{\omega}_y = 0$

$\frac{\dot{\omega}_x}{\dot{\omega}_y} = -\frac{\omega_y}{\omega_x}$

Because no torque,

from Euler eq. $N_x = I_x \dot{\omega}_x + \omega_y \omega_z (I_z - I_y) = 0$
 $N_y = I_y \dot{\omega}_y + \omega_z \omega_x (I_x - I_z) = 0$

putting in $I_z = I_x + I_y$ in to the N_x

$\Rightarrow I_x \dot{\omega}_x + \omega_y \omega_z I_x = 0 \Rightarrow \dot{\omega}_x = -\omega_y \omega_z$

N_y eq. $\Rightarrow I_y \dot{\omega}_y + \omega_z \omega_x (-I_y) = 0 \Rightarrow \dot{\omega}_y = +\omega_z \omega_x$
 $\frac{\dot{\omega}_x}{\dot{\omega}_y} = \frac{-\omega_y \omega_z}{\omega_z \omega_x}$ divide

or

$\frac{\dot{\omega}_x}{\dot{\omega}_y} = -\frac{\omega_y}{\omega_x}$

$N_z = I_z \dot{\omega}_z + \omega_x \omega_y (I_y - I_x) = 0$

for $I_y \neq I_x$

$= I_z \dot{\omega}_z + \omega_x \omega_y (I_y - I_x) = 0$

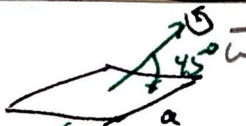
not const
 if not a principal axis

so $I_z \dot{\omega}_z = \text{varying}$
 $\Rightarrow \omega_z \neq \text{const}$

precession

unless $I_y = I_x$ then $I_z \dot{\omega}_z + 0 = 0 \Rightarrow \omega_z = \text{const}$

8.11.


 about $\hat{z}$
about $\hat{I}$

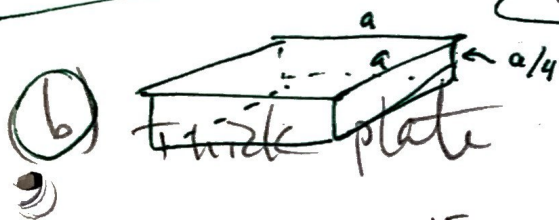
(a) $\Omega = \omega \left[\frac{I_s}{I} - 1 \right] \cos \alpha$; $\dot{\varphi} = \omega \left[1 + \left(\frac{I_s}{I} - 1 \right) \cos^2 \alpha \right]^{\frac{1}{2}}$

Find period of precession

Thin plate $I_s = \frac{1}{6} a^2$, $I = \frac{a^2}{12}$

so $T_{\Omega} = \frac{2\pi}{\Omega} = \frac{2\pi}{\omega} \frac{1}{\frac{1}{12} \left[\frac{1}{6} - 1 \right]} = \frac{2\pi\sqrt{2}}{\omega}$ ✓

$T_{\dot{\varphi}} = \frac{2\pi}{\dot{\varphi}} = \frac{2\pi}{\omega} \frac{1}{\left[1 + \left(\frac{\frac{1}{6} a^2}{\frac{1}{12} a^2} - 1 \right) \frac{1}{2} \right]^{\frac{1}{2}}} = \frac{2\pi}{\omega} \frac{1}{\left[\frac{5}{2} \right]^{\frac{1}{2}}} = \frac{2\pi(2)}{\omega(5)^{\frac{1}{2}}} = \frac{2\pi(2)}{\omega(5)^{\frac{1}{2}}}$ ✓



(b) thick plate $I_s = \frac{a^2}{6}$, $I = \frac{a^2 + c^2}{12}$ but $c = \frac{a}{4}$

so $I = \frac{15 \cdot 16}{16 \cdot 12} = \frac{5}{16 \cdot 4} = \frac{5}{64} a^2$

$T_{\Omega} = \frac{2\pi}{\Omega} = \frac{2\pi}{\omega} \frac{1}{\left[\frac{\frac{a^2}{6}}{\frac{5}{64} a^2} - 1 \right] \frac{1}{\sqrt{2}}} = \frac{2\pi\sqrt{2}}{\omega} \frac{30}{64 - 30} = \frac{2\pi\sqrt{2}}{\omega} \frac{15}{17} = \frac{34\sqrt{2}\pi}{15\omega}$

$T_{\dot{\varphi}} = \frac{2\pi}{\dot{\varphi}} = \frac{2\pi}{\omega} \frac{1}{\left[1 + \left\{ \left(\frac{\frac{a^2}{6}}{\frac{5}{64} a^2} \right)^2 - 1 \right\} \frac{1}{2} \right]^{\frac{1}{2}}} = \frac{2\pi}{\omega} \frac{1}{\left[1 + \left[\left(\frac{64}{30} \right)^2 - 1 \right] \right]^{\frac{1}{2}}}$

$= \frac{2\pi}{\omega} \left[\frac{600}{3796} \right]^{\frac{1}{2}} \approx \frac{1.33\pi}{\omega}$

$\frac{4096 - 900 + 200}{2 \cdot 300}$

8.13

Find the angle between $\vec{\omega}$ & $\vec{I}$ for two cases in #11

$$\chi = \alpha - \theta$$

$$\dot{\varphi} = \omega \frac{\sin \alpha}{\sin \theta}$$

$$\sin^{-1}\left(\frac{\omega}{\dot{\varphi}} \sin \alpha\right) = \theta$$

$$\chi = 45^\circ -$$

$$\tan^{-1}\left(\frac{I}{I_s} \tan \alpha\right)$$

a)

$$\chi = 45^\circ - \tan^{-1}\left(\frac{\frac{a^2}{12}}{\frac{a^2}{6}}(1)\right) = 45^\circ - \tan^{-1}\left(\frac{1}{2}\right) = 18.4^\circ$$

$$b) \chi = 45^\circ - \tan^{-1}\left(\frac{\frac{a^2}{12} + c^2}{\frac{a^2}{6}}(1)\right)$$

$$= 45^\circ - \tan^{-1}\left(\frac{17}{32}\right) = 17.02^\circ$$

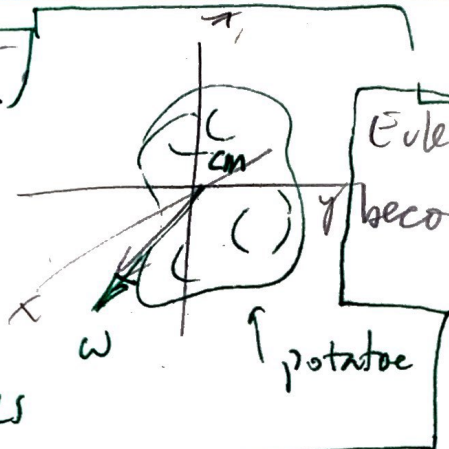
$$\chi = 45^\circ - \tan^{-1}\left(\frac{a^2 + c^2}{2a^2}\right) = 45^\circ - \tan^{-1}\left(\frac{1}{2} + \frac{c^2}{2a^2}\right)$$

Demonstrate the intermediate axis theorem

8.15

$$\text{let } I_z \gg I_y > I_x$$

10



No Torques

Euler's

become

$$\dot{\omega}_x = -\omega_y \omega_z (I_z - I_y) / I_x$$

$$\dot{\omega}_y = -\omega_z \omega_x (I_x - I_z) / I_y$$

$$\dot{\omega}_z = -\omega_x \omega_y (I_y - I_x) / I_z$$

I_{middle}

I_{big}

I_{small}

if $\vec{\omega} \parallel \hat{x}$ and displaced a little, $\Delta \omega$

$$\text{then } \dot{\omega}_x = -(\omega_y + \Delta \omega_y)(\omega_z + \Delta \omega_z) I_m \approx 0$$

$$\dot{\omega}_y = -(\omega_z + \Delta \omega_z)(\omega_x + \Delta \omega_x) I_b$$

$$\dot{\omega}_z = -(\omega_x + \Delta \omega_x)(\omega_y + \Delta \omega_y) I_s$$

stable

(ω_x will change

drastically)

$\vec{\omega} \parallel \hat{y}$

$$\dot{\omega}_x = -(\omega_y + \Delta \omega_y)(\omega_z + \Delta \omega_z) I_m \text{ small}$$

$$\dot{\omega}_y = -(\omega_z + \Delta \omega_z)(\omega_x + \Delta \omega_x) I_b \text{ Big}$$

$$\dot{\omega}_z = -(\omega_x + \Delta \omega_x)(\omega_y + \Delta \omega_y) I_s$$

unstable.

(oh well)

please see the key

8.15) Euler's equations for zero torque:

$$I_i \dot{\omega}_i + \omega_j \omega_k (I_k - I_j) = 0 \quad (i, j, k) = \text{cyclic permutation of } (x, y, z)$$

$$(I_x = I_{xx}, I_y = I_{yy}, I_z = I_{zz})$$

$$\Rightarrow \dot{\omega}_i = - \omega_j \omega_k \frac{(I_k - I_j)}{I_i}$$

Three solutions to these equations are

$$\omega_i = \text{constant}, \quad \omega_j = \omega_k = 0.$$

To examine stability, assume we are very close to one of these solutions, so $\omega_i = \omega_0 + \epsilon_i$, $\omega_j = \epsilon_j$, $\omega_k = \epsilon_k$.

The ϵ 's are small, so we can neglect ϵ^2 terms.

For simplicity of notation take $i, j, k = x, y, z$ now.

$$\Rightarrow \dot{\omega}_x = \dot{\epsilon}_x = - \epsilon_y \epsilon_z \left(\frac{I_z - I_y}{I_x} \right) \approx 0$$

$$\dot{\omega}_y = \dot{\epsilon}_y \approx - \epsilon_z \omega_0 \left(\frac{I_x - I_z}{I_y} \right)$$

$$\dot{\omega}_z = \dot{\epsilon}_z \approx - \omega_0 \epsilon_y \left(\frac{I_y - I_x}{I_z} \right)$$

$$\text{Solve the last equation for } \epsilon_y: \quad \epsilon_y \approx - \frac{I_z \dot{\epsilon}_z}{\omega_0 (I_y - I_x)}$$

$$\Rightarrow \dot{\epsilon}_y \approx - \frac{I_z \ddot{\epsilon}_z}{\omega_0 (I_y - I_x)}$$

$$\Rightarrow \ddot{\epsilon}_z = \epsilon_z \omega_0^2 \frac{(I_y - I_x)(I_x - I_z)}{I_y I_z}$$

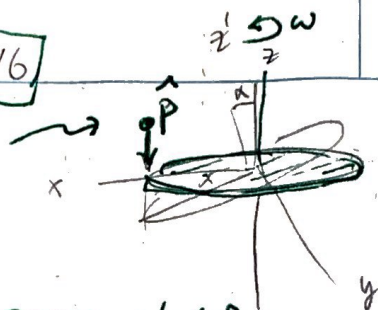
$$\text{and, similarly, } \ddot{\epsilon}_y = \epsilon_y \omega_0^2 \frac{(I_y - I_x)(I_x - I_z)}{I_y I_z}$$

So ϵ_y and ϵ_z are subject to a linear restoring force producing stability if $(I_y - I_x)(I_x - I_z) < 0$.

$\therefore$ Stable if I_x is greatest or smallest principle moment of inertia.
Unstable if I_x is between the other two.

8.16

meteor



space platform

Find resulting motion after the meteor strikes platform

by conservation of angular momentum

$$\hat{N}_y = rF = \frac{d\hat{L}}{dt}$$

during Δt :

$$N_y = I\dot{\omega}_y = aF = a \frac{\hat{p}}{\Delta t}$$

$$\dot{\omega}_y \Delta t = \frac{a\hat{p}}{I}$$

$$\int_0^{\Delta\omega_{y,\max}} d\omega_y = \int_0^{\Delta t} \frac{aF dt}{I}$$

$$\underline{\underline{\dot{\omega}_y}} = \frac{aF\Delta t}{I} = \underline{\underline{\frac{a\hat{p}}{I}}}$$

$$\sin \alpha_{\max} = \frac{\Delta z}{a} = \frac{\frac{1}{2} a \dot{\omega}_y \Delta t^2}{a} = \frac{1}{2} \dot{\omega}_y \Delta t^2$$

$$\alpha = \sin^{-1} \left(\frac{1}{2} \dot{\omega}_y \Delta t^2 \right)$$

We assume spin remains the same: i.e. $\omega_z' = \omega_z = \omega$

$$z' \text{ precesses about } z \text{ by } \Omega = \left(\frac{I_z}{I} - 1 \right) \omega_z' \cos \alpha$$

$$\underline{\underline{\Omega}} = (1) \omega \cos \left(\sin^{-1} \left(\frac{1}{2} \dot{\omega}_y \Delta t^2 \right) \right) = \omega \sqrt{1 - \frac{\dot{\omega}_y^2 \Delta t^4}{4}} = \omega \sqrt{1 - \frac{a^2 \hat{p}^2 \Delta t^2}{I^2}}$$

 z precess about a fixed vertical axis (invariable line)

$$\begin{aligned} \underline{\underline{\dot{\phi}}} &= \omega (1 + 3 \cos^2 \alpha)^{1/2} = \omega (1 + 3(1 - \frac{1}{4} \dot{\omega}_y^2 \Delta t^4))^{1/2} \\ &= \underline{\underline{\omega (1 + 3(1 - \frac{1}{4} \frac{a^2 \hat{p}^2}{I^2} \Delta t^2))^{1/2}}} \end{aligned}$$

please see the key

8.16) $\hat{P} = \hat{P} \hat{k}$, $\hat{L} = -\hat{P} a \hat{j}$ if the impulse is imparted on the x-axis at $a \hat{i}$.

$$\underline{\Delta \vec{v}_{cm} = \frac{\hat{P}}{m} \hat{k}}$$

$$\Delta \vec{L} = \hat{L}$$

$$\vec{L}_{initial} = \underline{I} \omega \hat{k} \quad \underline{I} = \begin{pmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 2 \end{pmatrix} \frac{ma^2}{4} \quad \omega \hat{k} = \begin{pmatrix} 0 \\ 0 \\ \omega \end{pmatrix}$$

$$\Rightarrow \vec{L}_{initial} = \frac{m\omega a^2}{2} \hat{k}$$

$$\vec{L} = \vec{L}_{initial} + \hat{L} = \underline{\frac{m\omega a^2}{2} \hat{k} - \hat{P} a \hat{j}} \quad \text{immediately after impulse}$$

Subsequent motion is torque free.

$$\Rightarrow I \dot{\omega}_x + \omega_y \omega_z (I_z - I) = 0$$

$$I \dot{\omega}_y + \omega_z \omega_x (I - I_z) = 0$$

$$I_z \dot{\omega}_z = 0$$

$$\vec{L} = \frac{ma^2}{4} \omega_x \hat{i} + \frac{ma^2}{4} \omega_y \hat{j} + \frac{ma^2}{2} \omega_z \hat{k}$$

$$\Rightarrow \omega_x = 0, \quad \omega_y = -\frac{4\hat{P}}{ma}, \quad \omega_z = \omega. \quad \text{immediately after the meteorite hits.}$$

$$\omega_z = \text{const.} = \omega.$$

$$\Omega = \omega$$

$$\omega_x = +\frac{4\hat{P}}{ma} \sin \Omega t = +\frac{4\hat{P}}{ma} \sin \omega t$$

$$\omega_y = -\frac{4\hat{P}}{ma} \cos \Omega t = -\frac{4\hat{P}}{ma} \cos \omega t$$

$$\tan \alpha = \frac{4\hat{P}}{ma\omega}$$

$$\dot{\phi} = \sqrt{\omega^2 + \frac{16\hat{P}^2}{m^2 a^2}} \sqrt{1 + 3 \cos^2 \alpha}$$

8.21

diam = b

① $\omega = ?$ to keep the pencil upright?
pencil spins in upright position

we let $n_3 = 1$ so $\alpha = \omega \theta$ $\theta = 0$

stability:

$$S^2_{\text{pin}} > \frac{4I_m g \left(\frac{a}{2}\right)}{I_s^2}$$

$$\text{or } S^2 > \left(\frac{4 m g \left(\frac{a}{2}\right) \left(\frac{b^2}{16} + \frac{a^2}{12}\right) m}{m^2 \frac{(b^2)^2}{64}} \right)$$

$$> \underline{128 a g \left(\frac{1}{16} + \frac{a^2}{b^2 12}\right)} \text{ close}$$

⑥ for $a = 20$ $b = 1$

$$S \approx 128 (20) (980) \left(\frac{20^2}{12}\right) \text{ R/sec.}$$

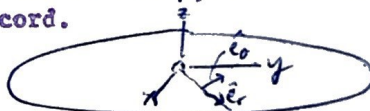
$\approx$

$$S > 1.7 \times 10^5 \text{ rpm}$$

Due: 1:10 p.m., Oct. 19

Open book - you may use your text, notes, and problem solutions.
You may also use math tables. You may not use any other books or consult with anyone except Dr. Evenson.

- (10) 1. A bug walks with constant speed v outward from the center along a radius of a phonograph record which is turning with constant angular velocity ω . The coefficient of friction between bug and record is μ . At what radius will the friction force first fail to supply the needed centripetal acceleration? Do this problem in a coordinate system fixed to the record.



$$\vec{r} = r \hat{e}_r$$

$$\dot{\vec{r}} = \dot{r} \hat{e}_r + r \dot{\theta} \hat{e}_\theta$$

$$\dot{\theta} = 0$$

$$\ddot{\vec{r}} = \ddot{r} \hat{e}_r$$

$$\ddot{\vec{r}} = (\ddot{r} - r \dot{\theta}^2) \hat{e}_r + (2\dot{r}\dot{\theta} + r\ddot{\theta}) \hat{e}_\theta = 0$$

$$\ddot{\vec{r}} = 0$$

$$\vec{\omega} = \omega \hat{k}$$

$$\vec{A}_0 = 0$$

$$\ddot{\vec{R}} = \ddot{\vec{r}} + \vec{A}_0 + 2\vec{\omega} \times \dot{\vec{r}} + \dot{\vec{\omega}} \times \vec{r} + \vec{\omega} \times (\vec{\omega} \times \vec{r})$$

$$\ddot{\vec{A}} = \ddot{\vec{R}} = 0 + 0 + 2(\omega \hat{k} \times v \hat{e}_r) + 0 + \omega \hat{k} \times (\omega \hat{k} \times r \hat{e}_r)$$

$$\ddot{\vec{R}} = 2\omega v \hat{e}_\theta - \omega^2 r \hat{e}_r$$

$$\vec{F}_f = m \ddot{\vec{R}} = \mu m g \frac{\ddot{\vec{R}}}{|\ddot{\vec{R}}|}$$

$$|\ddot{\vec{R}}| = \mu g = \sqrt{(2\omega v)^2 + (-\omega^2 r)^2}$$

$$\omega + \frac{\sqrt{(\mu g)^2 - 4\omega^2 v^2}}{\omega^2} = r$$

$$\sqrt{\frac{(\mu g)^2 - 4\omega^2 v^2}{\omega^4}} = r$$